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ERRATUM

Momentum fluxes in wind-forced breaking waves – ERRATUM

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The publisher apologises that, upon publication of this article (Scapin *et al.* 2025), several typographical errors were introduced by the typesetters during the production process. These affect Figure 8 (specifically panel b and the caption), Figure 9 (specifically the caption), and Figure 11 (specifically panel b). The correct versions of Figures 8, 9, and 11 are reported in figures 1, 2, and 3, respectively.

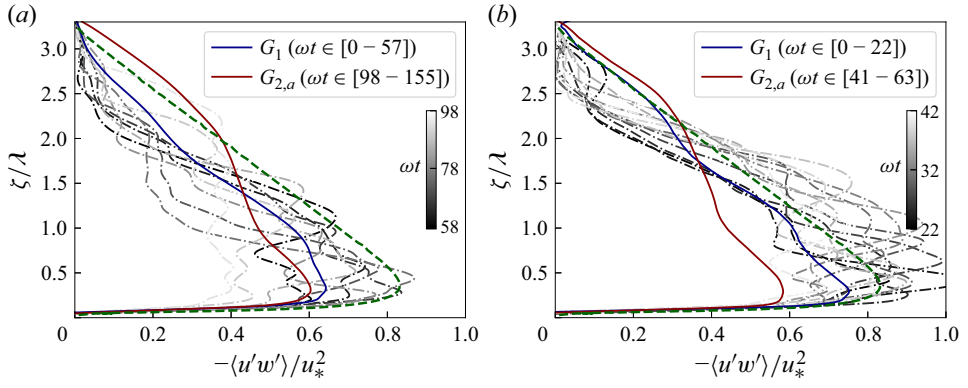


Figure 1. Reynolds shear stress normalized by the square of the nominal friction, $-\langle u'w'\rangle/u_*^2$, as a function of the vertical wave-following coordinate ζ for: (*a*) $u_*/c = 0.5$ and (*b*) $u_*/c = 0.9$. The Reynolds shear stress is averaged over the same time windows as in figure 7 of the published article Scapin *et al.* (2025). The dot-dashed curves represent the instantaneous values during the breaking stage, i.e. $\omega t \in [58-98]$ for $u_*/c = 0.5$ and $\omega t \in [22-42]$ for $u_*/c = 0.9$. The dashed green curve represents the Reynolds stress on a flat stationary surface at $Re_* = 720$.

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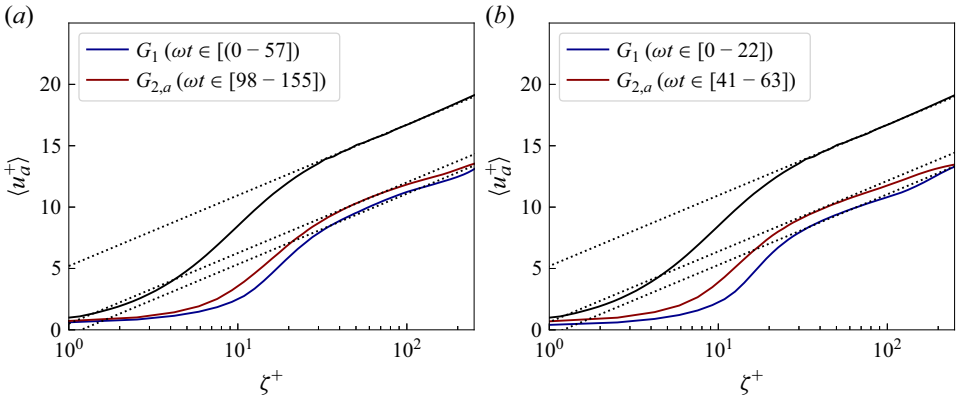


Figure 2. Streamwise velocity profile normalized by the friction velocity, $\langle u_a^+ \rangle = \langle u_a \rangle / u_*$, as a function of vertical wave-following coordinate (in wall units) $\zeta^+ = \zeta u_* / \nu_a$ with $\nu_a = \mu_a / \rho_a$: (*a*) $u_*/c = 0.5$ and (*b*) $u_*/c = 0.9$, both at $Re_{*,\lambda} = 214$ ($Re_* = 720$). The velocity profiles are averaged over the same time windows as in figure 7 of the published article Scapin *et al.* (2025). The dotted black lines refer to the fitted log law employed to estimate the intercept for each case. The continuous black line represents the mean velocity profile at $Re_* = 720$ for a flat stationary surface.

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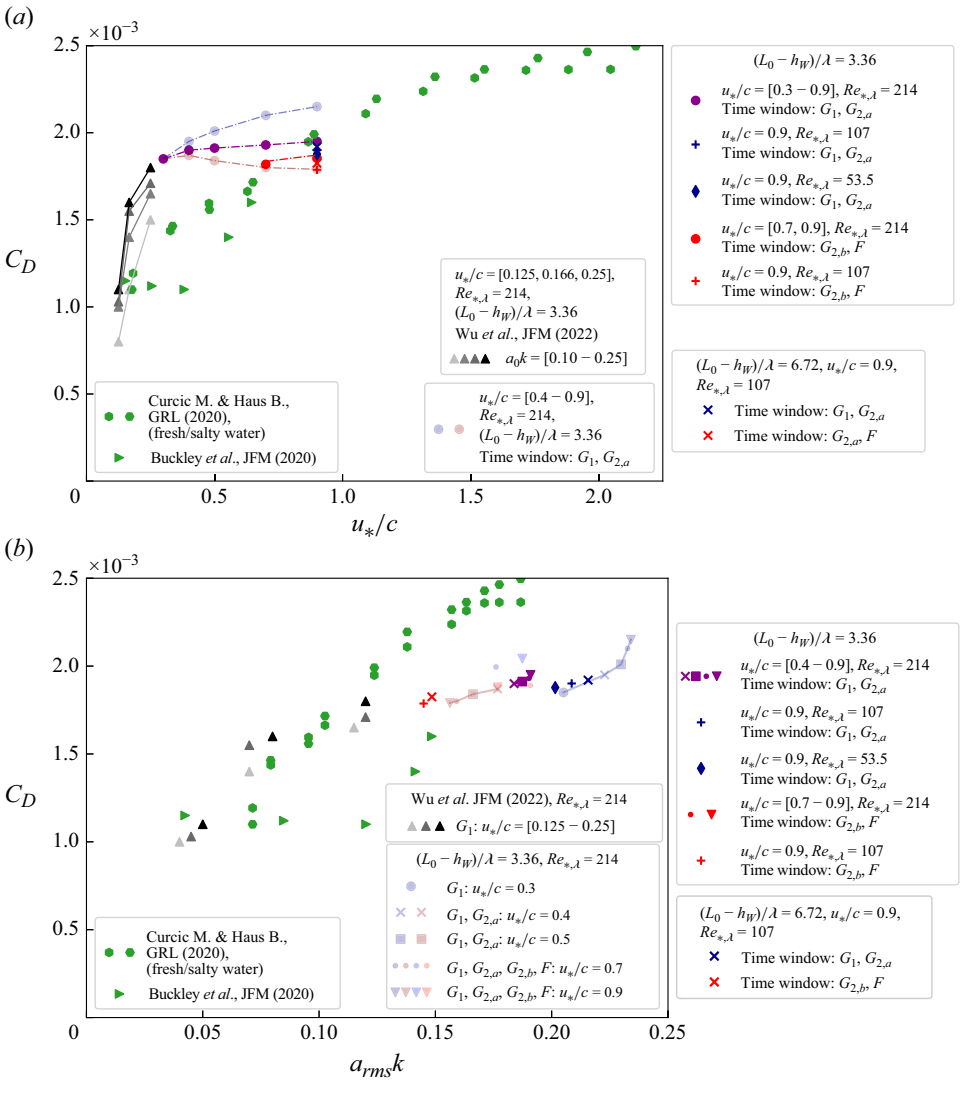


Figure 3. Drag coefficient C_D evaluated at $\overline{z} = 10$ m using equation 5.3 of the published article Scapin *et al.* (2025) as a function of u_*/c (top) and $a_{rms}k$ (bottom) with $a_{rms} = a/\sqrt{2}$. The figure includes the calculation of C_D with the data generated in this work and the one retrieved from Wu *et al.* (2022). For all the cases, the reported C_D is an average value between the first growing cycle, G_1, and a fraction of the second growing cycle, $G_{2,a}$ (immediately after the breaking event). Whenever available, the data pertaining to the second growing cycle $G_{2,b}$ and the final stage F are displayed. The employed time window to define C_D follows the convention given in figure 3(*b*) of the published manuscript (Scapin *et al.* 2025). For the cases at $u_*/c = [0.4 - 0.5 - 0.7 - 0.9]$ at $Re_{*,\lambda} = 214$ with $(L_0 - h_W)/\lambda = 3.36$, we separate between these two stages (blue and red dots). The green symbols display the experimental datasets from Buckley *et al.* (2020) up to $u_*/c \approx 0.71$ and from Curcic & Haus (2020) up to $u_*/c \approx 2.25$.

Reference

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