International Journal of Microwave and Wireless Technologies

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Prediction on operating range of passive troposcatter detection system

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Research Paper

Cite this article: Liu Z, Chen X (2019). Prediction on operating range of passive troposcatter detection system. *International Journal of Microwave and Wireless Technologies* **11**, 22–26. https://doi.org/10.1017/S1759078718001411

Received: 4 May 2018
Revised: 7 October 2018
Accepted: 9 October 2018
First published online: 5 November 2018

Key words:
Operating range; passive troposcatter detection system; propagation loss; tropospheric refractivity

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Abstract

Electromagnetic wave of enemy radar propagated by troposcatter is a valuable candidate for beyond line-of-sight detection. There is no analytical study considering the operating range of passive troposcatter detection system. In this paper, we study the way to predict the operating range, which is dominated by propagation loss. The key propagation loss models including statistic model and real-time model are analyzed. During deducing the latter loss model, Hopfield model is introduced to precisely describe the tropospheric refractivity. Meanwhile, rain attenuation is also taken into consideration. Several examples demonstrate the feasibility of predicting operating range through the proposed method.

Introduction

Effectively detecting the enemy early warning radar is vital. Satellite system can realize the beyond line-of-sight (b-LoS) detection. However, it has security problems and may be interrupted by the hostile jamming. Furthermore, satellite system generally uses the image recognition technology to search its targets, which is relatively powerless to detect the radiation sources in disguise or in blind areas [1]. Troposcatter is a promising candidate for the b-LoS propagation. Electromagnetic (EM) wave of hostile radar propagated by troposcatter can be utilized for the b-LoS detection [2–5].

To improve the maneuverability of passive troposcatter detection system, [2] has designed a receiving antenna mode based on the signal group delay. This mechanism can conveniently and inexpensively locate targets on the basis of only single station rather than multi-stations. High propagation loss is one of the main characteristics of troposcatter. In [3], a comprehensive method for predicting propagation loss has been presented. Troposcatter is also marred by the multipath fading, [4] has studied troposcatter transfer function, and proposed a fading correlation model to handle the signal received by the array antenna.

Although the passive troposcatter detection system has been well studied, there is no analytical study on the operating range, which is also an important factor in radar system. Estimating propagation loss is a key step to predict the operating range; the statistical propagation loss model is firstly analyzed in this paper. According to the existing researches [4, 5], time-varying meteorological parameters have obvious effect on tropospheric refractivity, which dominates the performance of troposcatter links. To estimate the dynamic operating range, the specific relationship between propagation loss and refractivity is presented. Furthermore, Hopfield model is introduced to precisely describe the refractivity at any altitude. Finally, we predict the operating range according to above discussion. The chief innovations of this paper are mainly focused on twofold. On the one hand, we innovatively predict the operating range of passive troposcatter detection system. On the other hand, operating range is predicted through dynamic loss model, instead of the conventional model.

In this paper, we study the operating range of passive troposcatter detection system; the characteristics of troposcatter including propagation loss and refractivity are also presented. The rest of this paper is organized as follows. Way to predict the operating range as well as different propagation loss models are given in "Operating range of passive detection system" section. In "Example analysis" section, some examples are displayed. "Conclusions" section draws the conclusion.

Operating range of passive detection system

Figure 1 shows the principle of passive troposcatter detection system. EM wave of enemy radar propagated by troposcatter can be detected by our system. Current signal detection algorithms mainly focus on matched filter detection, cyclostationary feature detection, and energy detection (ED) [5]. Different from cooperative occasions, passive system probably lacks priori knowledge on the targets [6]. ED which has simpler implementation and less requirement of priori knowledge is a preferred candidate for passive troposcatter detection system. Energy level of the received signal dominates the consequence of ED. Namely, key to predict

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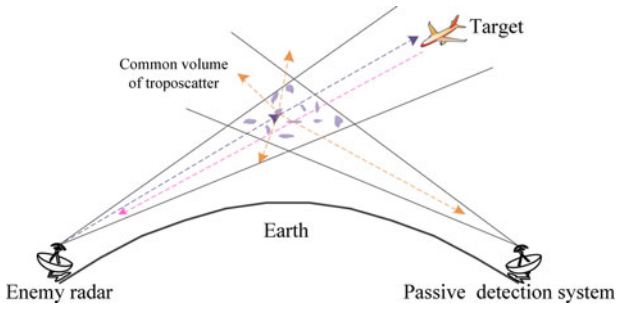


Fig. 1. Passive troposcatter detection system.

the operating range lies in estimating the received power, which can be given as

$$P_r = P_t - L_\Sigma, \tag{1}$$

where P_t denotes the transmitting power of enemy radar, P_r represents the power received by detection system, L_Σ is the propagation loss, which has obvious relationship with the distance between detection system and enemy radar. Only $P_r \geq S$, the detection system can work normally, here S is the receiver sensitivity. Hence we can estimate the operating range through the equation: $P_r = S$. Precisely calculating L_Σ is vital to predict the operating range.

Statistic propagation loss model

Several statistic models for estimating the propagation loss have been proposed. Zhang model has been internationally accepted [7]. The main propagation loss of a troposcatter channel can be given as

$$L = F + 30\lg f + 30\lg\Theta_0 + 10\lg d + 20\lg(5 + \gamma H) + 4.34\gamma h_0 + L_c, \tag{2}$$

where Θ_0 refers to the least scatter angle (mrad), which can be calculated as $\Theta_0 = \theta_t + \theta_r + 1000d/a_e$, here, a_e is the median effective earth radius. θ_t, θ_r are the transmitter and receiver horizon angle, respectively. F denotes the meteorological parameter (dB), γ represents the atmospheric structure coefficient (km^{-1}), f denotes the frequency (MHz), d refers to the path length between the receiving and transmitting antennas (km). H denotes the height between the lowest scattering point and the connection between receiving and transmitting antennas (km), which can be expressed as $H = 10^{-3}\Theta_0 d/4$. h_0 represents the height between the lowest scattering point and ground (km), which can be calculated as $h_0 = 10^{-6}\Theta_0^2 a_e/8$.

The aperture-to-medium coupling loss of an antenna [8] can be generally expressed as

$$L_c = 0.07 \times e^{0.055\times(G_t+G_r)}, \tag{3}$$

where G_t, G_r stand for the plane wave gains of TX/RX antennas, respectively. Both of them can be given as

$$G_{t,r} = 10\lg[4.5 \times (D/\lambda)^2], \tag{4}$$

where D denotes the antenna diameter. Therefore, L_Σ can be finally calculated as

$$L_\Sigma = L - (G_T + G_R). \tag{5}$$

Table 1. Information of three observations

Name	Longitude/°	Latitude/°	Elevation/m
WUHN	114.21	30.31	40.20
BJFS	115.89	39.61	98.30
XIAN	108.90	34.18	498.50

Although Zhang model can effectively estimate the propagation loss, the time resolution and spatial resolution are relatively poor.

Dynamic propagation loss model

The received power of a troposcatter link can be defined as [5, 9]

$$P_r = P_t \int_V \frac{\lambda^2 G_T G_R \sigma_v \rho}{(4\pi)^3 (r_1 r_2)^2} dV, \tag{6}$$

where λ denotes the wavelength, r_1 (r_2) represents the distance between the scatter point to $TX(RX)$, σ_v is the scattering cross-section. ρ denotes the aperture-to-medium coupling factor, which can be expressed as $L_c = -10\lg\rho$. V refers to the common volume, which can be approximated as

$$V = 1.206 \frac{r_1^2 r_2^2 \delta_t \delta_r \phi_t \phi_r}{\sqrt{r_1^2 \phi_t^2 + r_2^2 \phi_r^2 \sin\Theta}}, \tag{7}$$

where Θ is the scattering angle. $\delta_{t,r}$ denotes the half power beamwidth of transmitting and receiving antennas in the vertical direction. $\phi_{t,r}$ represents the half power beamwidth in the horizontal direction. They can be modeled as

$$\delta_{t,r}(\phi_{t,r}) = (70^\circ \sim 75^\circ) \times \lambda/D. \tag{8}$$

According to Kolmogorov theory, σ_v can be expressed as

$$\sigma_v = 2\pi k^4 = \sin^2 \chi^\Phi(K_s) \tag{9}$$

where $k = 2\pi/\lambda$ represents the wavenumber. $\chi = \pi/2$ for the horizontally polarized EM wave, $\chi = \pi/2 + \Theta$ for the vertically polarized EM wave. $\Phi(k_s)$ can be calculated as

$$\Phi(k_s) = 0.0033 k_s^{-m} C_n^2, \tag{10}$$

where $m = (11/3,5)$. Other parameters can be given as

$$\begin{cases} k_s = 2k\sin(\Theta/2) \\ C_n^2(\Lambda_0, M) = 2.8\Lambda_0^{4/3} M^2 \end{cases}, \tag{11}$$

where Λ_0 represents the outer scale of atmospheric turbulence, which can be written as

$$\Lambda_0(h) = \begin{cases} 0.4h, & 0 \leq h \leq 25\,\mathrm{m} \\ 2\sqrt{h}, & 25 \leq h \leq 1000\,\mathrm{m} \\ 63.24, & h \geq 1000\,\mathrm{m} \end{cases}. \tag{12}$$

In equation (11), M stands for the vertical gradient of tropospheric refractive index. According to the tropospheric theory,

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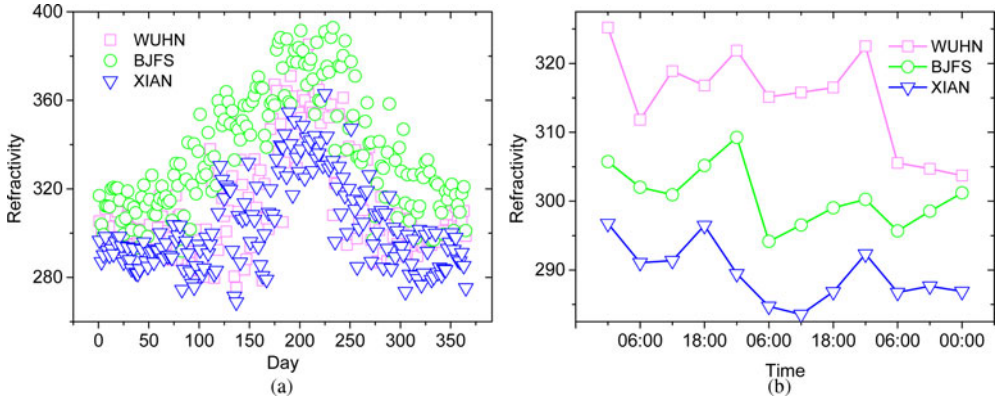


Fig. 2. Refractivity of three observations. (a) Refractivity of a year, (a) refractivity of 3 days.

$n = 1 + 10^{-6}N$, here, n, N refer to the tropospheric refractive index and refractivity, respectively. $N = N_{dry} + N_{wet}$ [10], here, N_{dry}, N_{wet} refer to the dry and wet terms of refractivity, respectively. Both of them can be expressed as [11]

$$\begin{cases} N_{dry} = 77.6P/T \\ N_{wet} = 373256e/T^2 \end{cases}, \tag{13}$$

where P denotes the atmospheric pressure in hPa, e represents the water vapor pressure in hPa, and T is the absolute temperature in K. Consequently, M can be deduced as

$$\frac{dn}{dh} = \frac{77.6}{10^6}\left[\frac{1}{T}\frac{dp}{dh} - \left(\frac{p}{T^2} + \frac{9620e}{T^3}\right)\frac{dT}{dh} + \frac{4810}{T^2}\frac{de}{dh}\right]. \tag{14}$$

As displayed in equation (14), estimating M through this way depends on precisely vertical gradient of meteorological parameters. ITU-R P. 835-5 gives a troposphere model based on latitude areas (low-latitude, mid-latitude, and high-latitude) and seasons (summer and winter) [12]. For example, model of mid-latitude area in summer can be expressed as

$$\begin{cases} T_{sum}(h) = 294.9838 - 5.2159h - 0.07109h^2 \\ P_{sum}(h) = 1012.8186 - 111.5569h + 3.864h^2 \\ \rho_{sum}(h) = 14.3542\exp[-0.4174h - 0.0229h^2 + 0.001007h^3] \\ e(h) = \rho(h)T(h)/216.7 \end{cases}, \tag{15}$$

where h denotes the altitude. Parameter M at any h can be estimated according to equation (14) and (15). However, both time resolution and spatial resolution are relatively poor, we cannot get the real-time refractivity through this model. Meteorological parameters of three observations in mid-latitude region are selected to display the change law of tropospheric refractivity. Table 1 displays the concrete information of these observations.

Figures 2(a) and 2(b) depict the refractivity of a whole year and first 3 days of a year, respectively. From Fig. 2, we can get that the refractivity of all observations is different and apparently changes with time. Namely, ITU model cannot describe the tropospheric refractivity in more detail. The refractivity model with better performance is in urgent need.

Table 2. Bias of propagation loss estimated by two models (dB)

Distance (km)	Climate zones						
	1	2	3	4	5	6	7
150	4.6	5.6	4.5	3.8	1.4	6.5	1.7
300	4.1	3.0	2.1	1.9	2.7	3.4	2.0
450	5.4	6.7	4.8	2.2	7.6	5.2	3.9

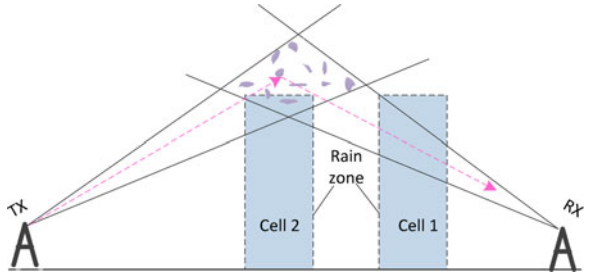


Fig. 3. Troposcatter communication in rain cell.

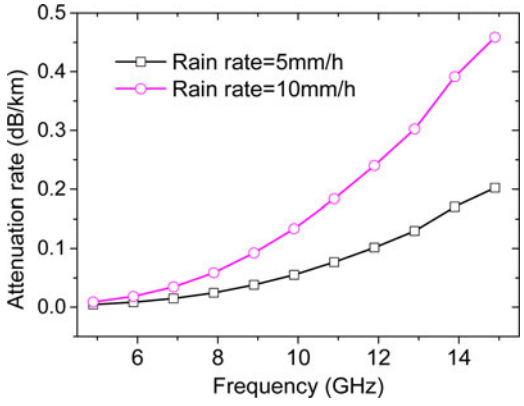


Fig. 4. Attenuation rate in rain cell.

Hopfield model [13] is widely used in satellite system, it can describe $N(h)$ as

$$N_i(h) = \frac{N_{i0}}{H_i^4}(H_i - h)^4 \quad i = \text{dry, wet}, \tag{16}$$

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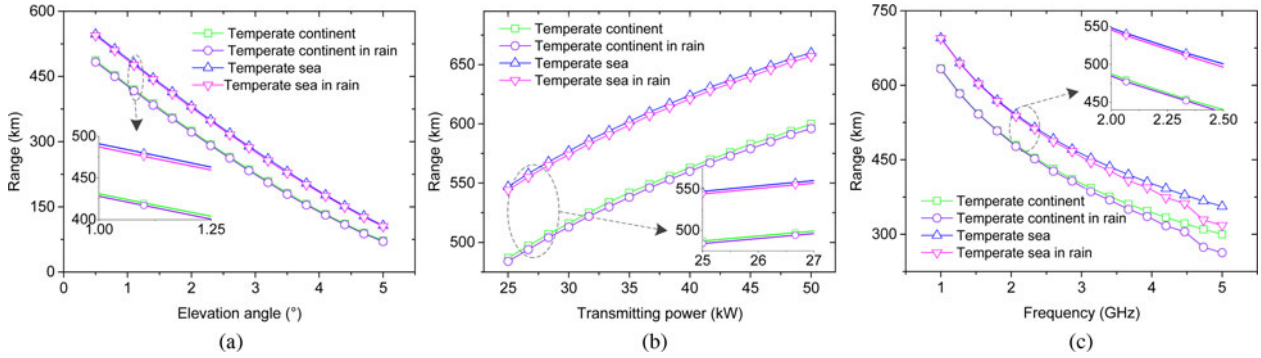


Fig. 5. Mean operating range of passive troposcatter detection system. (a) Operating range changing with θ_r; (b) operating range changing with P_t; (c) operating range changing with f.

where H_{dry}, H_{wet} denote the equivalent height for hydrostatic and wet refractivity, respectively. They can be given as

$$\begin{cases} H_{dry} = 40136 + 148.72(T_0 - 273.16)\text{m} \\ H_{wet} = 11\,000\,\text{m} \end{cases}. \tag{17}$$

The vertical gradient of tropospheric refractive index can be further deduced as

$$\frac{\partial n(h)}{\partial h} = \frac{-4}{10^6}\left[\frac{N_{dry0}}{H_{dry}^4}(H_{dry} - h)^3 + \frac{N_{wet0}}{H_{wet}^4}(H_{wet} - h)^3\right]. \tag{18}$$

According to equation (18), Hopfield model can directly estimate M through meteorological parameters of surface. It does not depend on vertical gradient of meteorological parameters. Ref. 14 employs several observations locating in different zones to show the performance of Hopfield model and ITU model. The consequences indicate that the former has obvious advantages. Table 2 shows bias of annual mean loss estimated by Zhang method and the time-varying method. Here, 1 stands for equator, 2 continental subtropical, 3 marine subtropical, 4 desert, 5 continental temperate, 6 sea, 7 marine temperate. Analogous consequences of different regions indicate that the dynamic method is logical. Detail information of climate zones is same as Fig. 1. Analogous consequences of two methods indicate that the latter method can also effectively estimate the propagation loss.

Rain attenuation model

Precipitation will affect the performance of many wireless links. Because the frequency of early warning radar always ranges in microwave bandwidth, rain has relatively obvious effect on the troposcatter link [15].

Figure 3 shows the troposcatter link under rain weather. Only the EM wave passing through rain cell will suffer from the additional attenuation. Without considering the rain scatter, the attenuation rate can be expressed as

$$\gamma_R = k \cdot R^{\gamma}\ \text{dB/km}, \tag{19}$$

where R denotes the rainfall rate (mm/h), k, γ are the empirical coefficients, the value of them can be found in ITU-R P.676-11 [16]. Figure 4 displays the γ_R changing with frequency. Rain attenuation becomes more obvious with the frequency increasing.

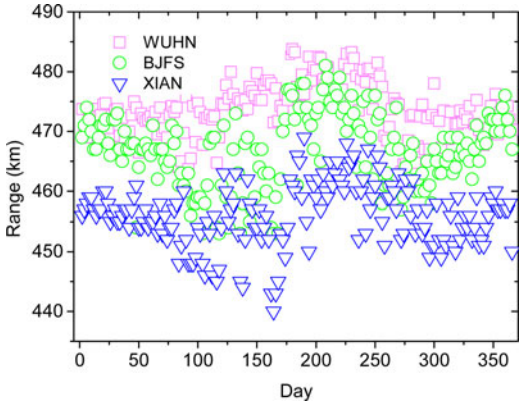


Fig. 6. Real-time operating range during a year.

Rain attenuation also depends on the length of wave passing in rain cell, [17] introduces a reasonable method.

As stated above, the received power follows

$$S = P_t - L_\Sigma - L_R, \tag{20}$$

where L_R denotes the rain attenuation. Operating range determines the propagation loss, it can be further deduced through equation (20).

Example analysis

In this section, some examples are analyzed. Figure 5(a) depicts annual mean range changing with θ_r under channel parameters: $f = 2$ GHz, $D_T = 10$ m, $D_R = 5$ m, $\theta_t = 1°$, $P_t = 25$ kW, $S = -90$ dBm. $R = 30$ mm/h, path length of EM wave passing through rain cell is 50 km. $\theta_r = 0.5°$, the other parameters are same as above, operating range changing with P_t and f is displayed in Figs 5(b) and 5(c), respectively.

From Fig. 5, the passive system can realize b-LoS detection. System located in the relatively moist area has further operating range. This phenomenon indicates that the moist atmosphere is beneficial for EM wave propagation. The undesirable effect caused by rain will be apparent with the frequency increasing. Parameters are same as above, real-time operating range during a year is shown in Fig. 6. The operating range during the whole year is different, and the maximum operating range appears in summer. Both Figs 5 and 6 demonstrate the feasibility of prediction on operating range of passive troposcatter detection system.

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Conclusions

In this paper, we predict the operating range of passive troposcatter detection system on the basis of propagation loss model. In addition, the dynamic propagation loss model improved by Hopfield model is proposed. According to our results, passive troposcatter detection system can realize b-LoS detection. As well, prediction on operating range is feasible, moist atmosphere is beneficial for passive troposcatter detection system.

Acknowledgements. We are grateful to Global Geodetic Observing System (GGOS) for providing the related meteorological data. We also gratefully acknowledge anonymous reviewers who read and make insightful and constructive suggestions. The authors declare that there is no conflict of interests regarding the publication of this paper. This work was supported by the National Natural Science Foundation of China under grand No. 61671468 and 61701525.

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